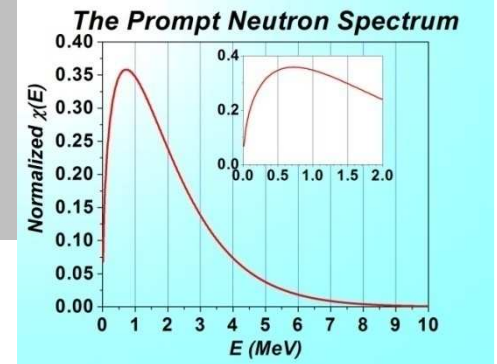


Controlled Fission

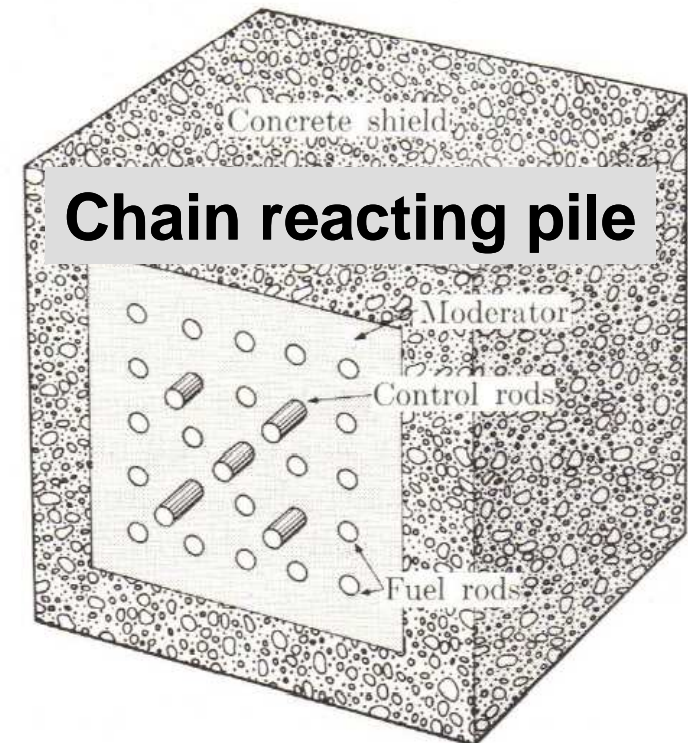


- $^{235}\text{U} + n \rightarrow X + Y + (\sim 2.4)n$ ← Fast second generation neutrons
- Moderation of second generation neutrons ► Chain reaction.
- Water, D_2O or graphite moderator.
- Ratio of number of “neutrons” (fissions) in one generation to the preceding $\equiv k_\infty$ (neutron reproduction or multiplication factor).

Infinite medium (ignoring leakage at the surface).

- $k \geq 1$ ► Chain reaction.
- $k < 1$ ► subcritical.
- $k = 1$ ► critical system.
- $k > 1$ ► supercritical.

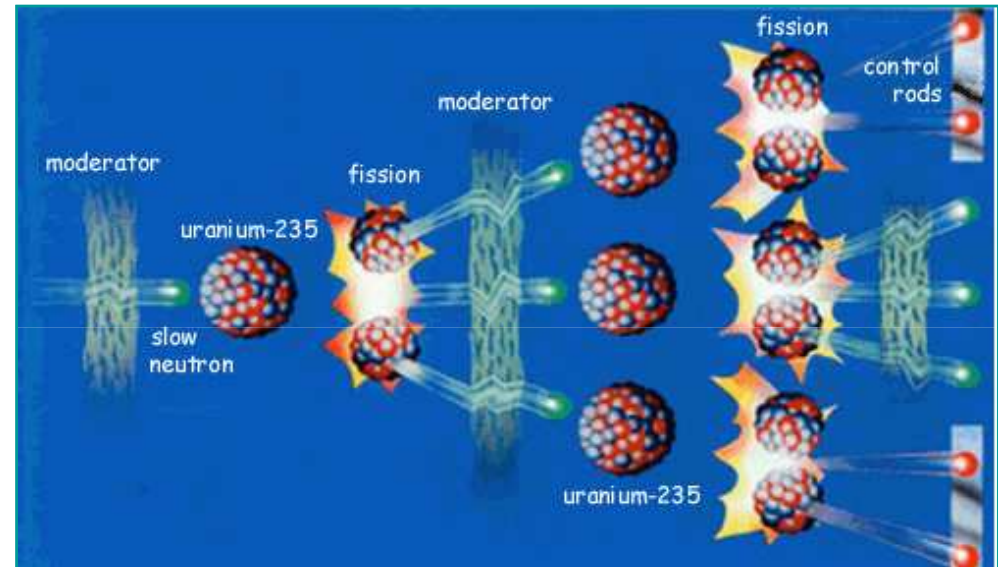
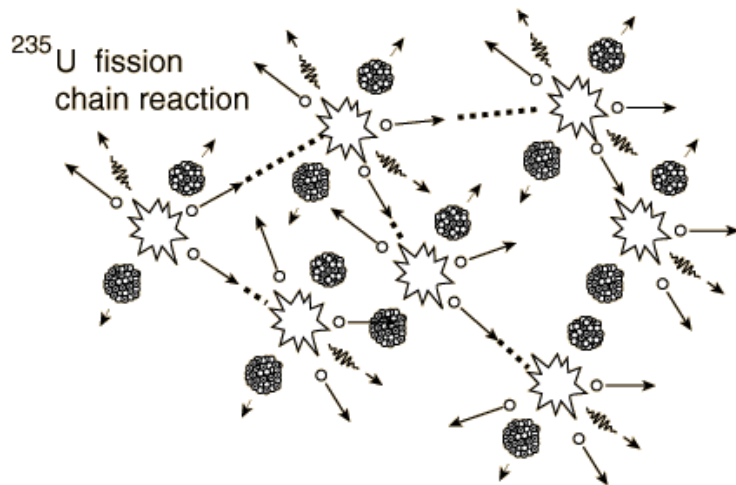
For steady release of energy (steady-state operation) we need $k = 1$.



Controlled Fission

- Average number of all neutrons released per fission
→ ν (for thermal neutrons, 0.0253 eV).
- ^{233}U : 2.492
- ^{235}U : 2.418
- ^{239}Pu : 2.871
- ^{241}Pu : 2.927

Fissile



Not all ν neutrons will subsequently cause fission...!

- Reactor is critical ($k = 1$): rate of neutrons produced by fission = rate of neutrons absorbed + leaked.

Controlled Fission

^{235}U thermal cross sections

$$\sigma_{\text{fission}} \approx 584 \text{ b.}$$

$$\sigma_{\text{scattering}} \approx 9 \text{ b.}$$

$$\sigma_{\text{radiative capture}} \approx 97 \text{ b.}$$

**Check
numbers!**



Probability for a thermal neutron to cause fission on ^{235}U is

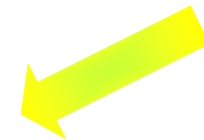
$$\approx \frac{\sigma_f}{\sigma_f + \sigma_\gamma} = \frac{1}{1 + \alpha}$$

Not all ν neutrons will subsequently cause fission...!

If each fission produces an average of ν neutrons, then the mean number of **fast** fission neutrons produced per thermal neutron = η

$$\eta = \nu \frac{\sigma_f}{\sigma_a} = \nu \frac{\sigma_f}{\sigma_f + \sigma_\gamma} = \frac{\nu}{1 + \alpha}$$

$$\eta < \nu$$



Controlled Fission

- **Assume natural uranium:**
99.2745% ^{238}U , 0.7200% ^{235}U .

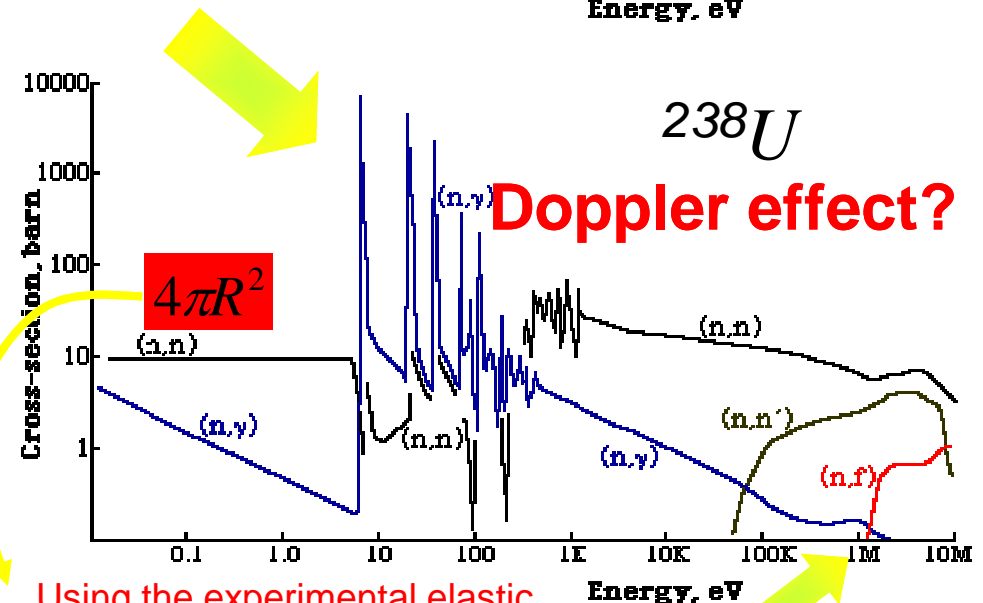
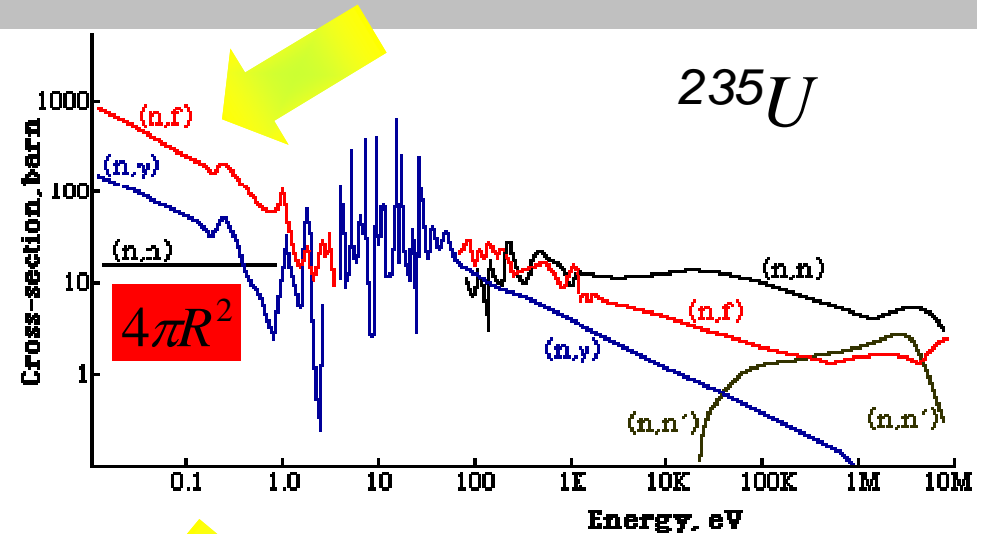
Thermal $\sigma_f = 0 \text{ b}$ Why? 584 b
 Thermal $\sigma_\gamma = 2.75 \text{ b}$ 97 b

$$\Sigma = \Sigma_x + \Sigma_y = N_x \sigma_x + N_y \sigma_y$$

$$= (\gamma_x \sigma_x + \gamma_y \sigma_y) N$$

- $\Sigma_f / N = (0.992745)(0) + (0.0072)(584) = 4.20 \text{ b.}$

- $\Sigma_\gamma / N = (0.992745)(2.75) + (0.0072)(97) = 3.43 \text{ b.}$



Using the experimental elastic scattering data the radius of the nucleus can be estimated.

Controlled Fission

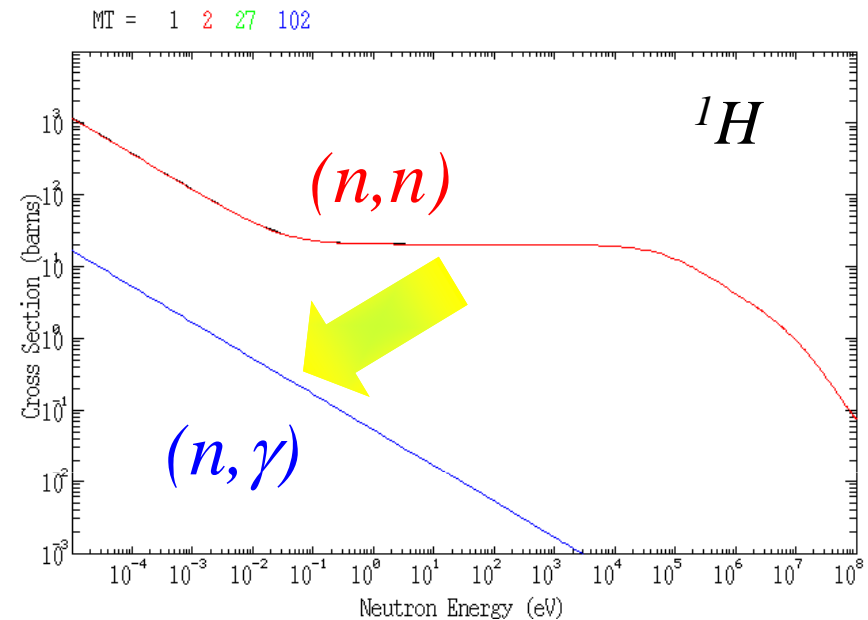
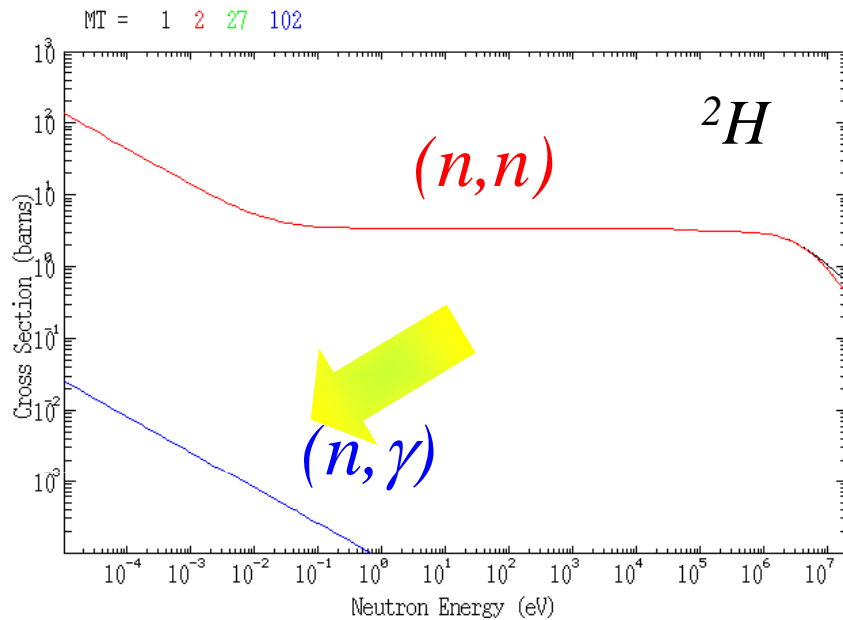
- Probability for a thermal neutron to cause fission in **natural uranium**

$$= \frac{4.20}{4.20 + 3.43} = 0.55$$

Compare to pure ^{235}U and to 3% enriched fuel.

- If each fission produces an average of $\nu = 2.4$ neutrons, then the mean number of fast fission neutrons produced per thermal neutron = $\eta = 2.4 \times 0.55 \approx 1.3$
- This is close to 1. If neutrons are still to be lost, there is a danger of losing criticality. (Heavy water?).
- For **enriched uranium** ($^{235}\text{U} = 3\%$) $\eta = \text{?????}$ (> 1.3). (Light water?).
- In this case η is further from 1 and allowing for more neutrons to be lost while maintaining criticality.

Moderation (to compare x-section)



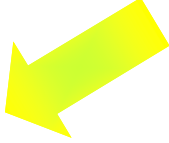
Timeout..!

- Resonances?
- 3H production.

Controlled Fission

HW 11

• Verify

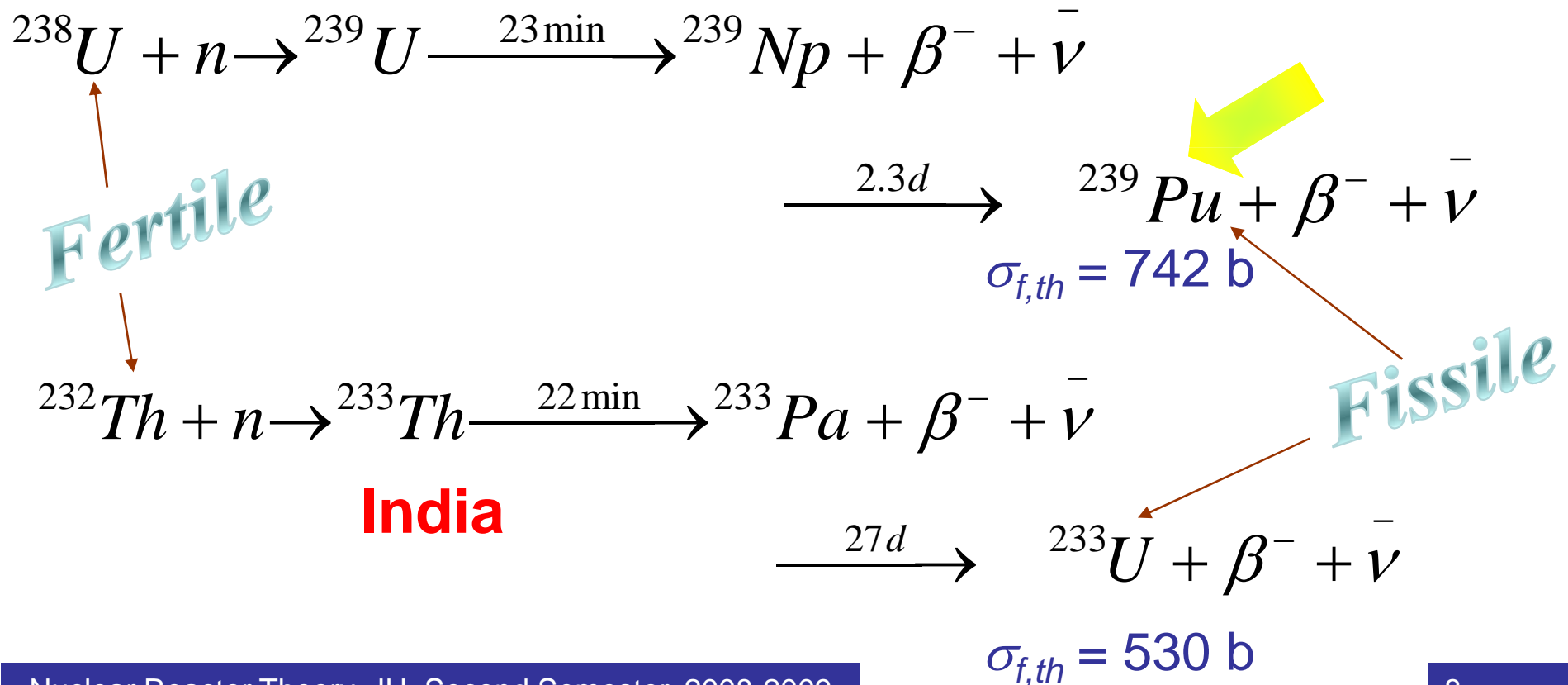
$$\eta = \frac{1}{\Sigma_a} \sum_i \nu(i) \Sigma_f(i)$$


- Comment on the calculation for thermal neutrons and a mixture of fissile and non-fissile materials, giving an example.
- Comment for fast neutrons and a mixture of fissionable materials, giving an example.

Conversion and Breeding

Timeout..!

Converters: Convert non-thermally-fissionable material to a thermally-fissionable material.



Conversion and Breeding

Timeout..!

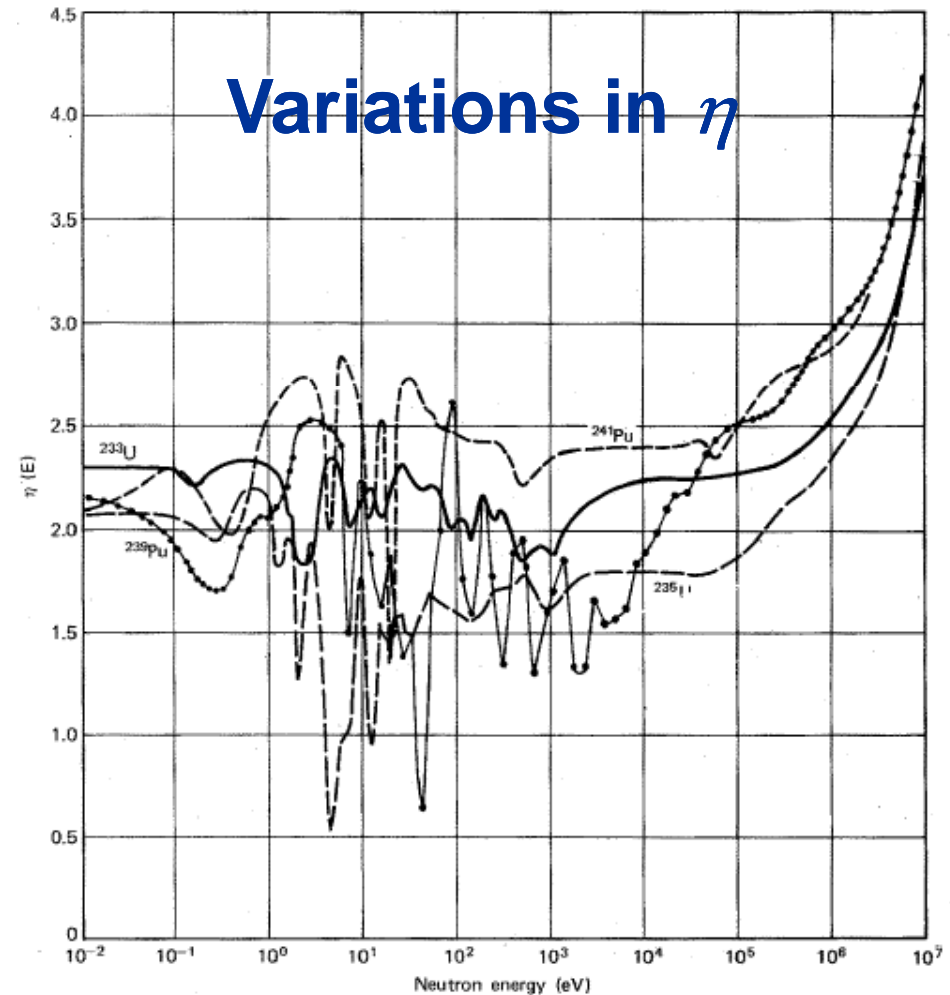
Delicate neutron economy....!

- If $\eta = 2$ ► Conversion and fission.
- If $\eta > 2$ ► Breeder reactor.
- ^{239}Pu : Thermal neutrons ($\eta \sim 2.1$) ► hard for breeding.
Fast neutrons ($\eta \sim 3$) ► possible breeding ► fast breeder reactors.
- After sufficient time of breeding, fissile material can be easily (chemically) separated from fertile material.
Compare to separating ^{235}U from ^{238}U .
- Reprocessing.

Controlled Fission

Timeout..!

- Note that η is greater than 2 at thermal energies and almost 3 at high energies.
- These “extra” neutrons are Used to convert fertile into fissile fuel.
- **Plutonium economy.**
- **India and thorium.**
- Efficiency of this process is determined by neutron energy spectrum.



Controlled Fission

Timeout..!

- **Conversion ratio** CR is defined as the average rate of fissile atom production to the average rate of fissile atom consumption.
- For LWR's $CR \cong 0.6$.
- CR is called BR for values > 1 .
- Fast breeder reactors have $BR > 1$.
- They are called “fast” because primary fissions inducing neutrons are fast not thermal, thus $\eta > 2.5$ but σ_f is only a few barns.
- Moderator??

Controlled Fission

- N **thermal** neutrons in one generation **have produced so far ηN fast neutrons.**
- Some of these **fast** neutrons can cause ^{238}U fission ► more fast neutrons ► **fast fission factor** = ε (= 1.03 for natural uranium).
- **Now we have $\varepsilon\eta N$ fast neutrons.**
- We need to moderate these fast neutrons ► use graphite as an example ► for 2 MeV neutrons we need ??? collisions. **How many for 1 MeV neutrons?**
- The neutron will pass through the 10 - 100 eV region during the moderation process. This energy region has many **strong** ^{238}U capture resonances (up to ????? b) ► Can not mix uranium and moderator.
- In graphite, an average distance of 19 cm is needed for thermalization ► the **resonance escape probability** p (≈ 0.9).

Controlled Fission

- **Now we have $p\varepsilon\eta N$ thermal neutrons.**
- Moderator must not be too large to capture thermal neutrons; **when thermalized, neutrons should have reached the fuel.**
- Graphite thermal cross section = 0.0034 b, but there is a lot of it present.
- Capture can also occur in the material encapsulating the fuel elements (clad).
- The **thermal utilization factor** f (≈ 0.9) gives the fraction of thermal neutrons that are actually available for the fuel.
- **Now we have $fp\varepsilon\eta N$ thermal neutrons**, could be $>$ or $< N$ thus determining the criticality of the reactor.

$$k_{\infty} = fp\varepsilon\eta \quad \text{The four-factor formula.}$$

$$k = k_{eff} = fp\varepsilon\eta(1-l_{fast})(1-l_{thermal})$$

Fractions lost at surface

Controlled Fission

$$k_{\infty} = fp\varepsilon\eta, \quad k_{eff} = f\rho\varepsilon\eta P_{non-leak}$$

- Fast from thermal, $\eta = \frac{1}{\Sigma_a} \sum_i \nu(i)\Sigma_f(i)$ as defined in HW 11.
- Fast from fast, ε .
- Thermal from fast, p .

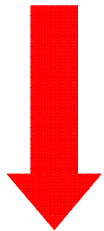
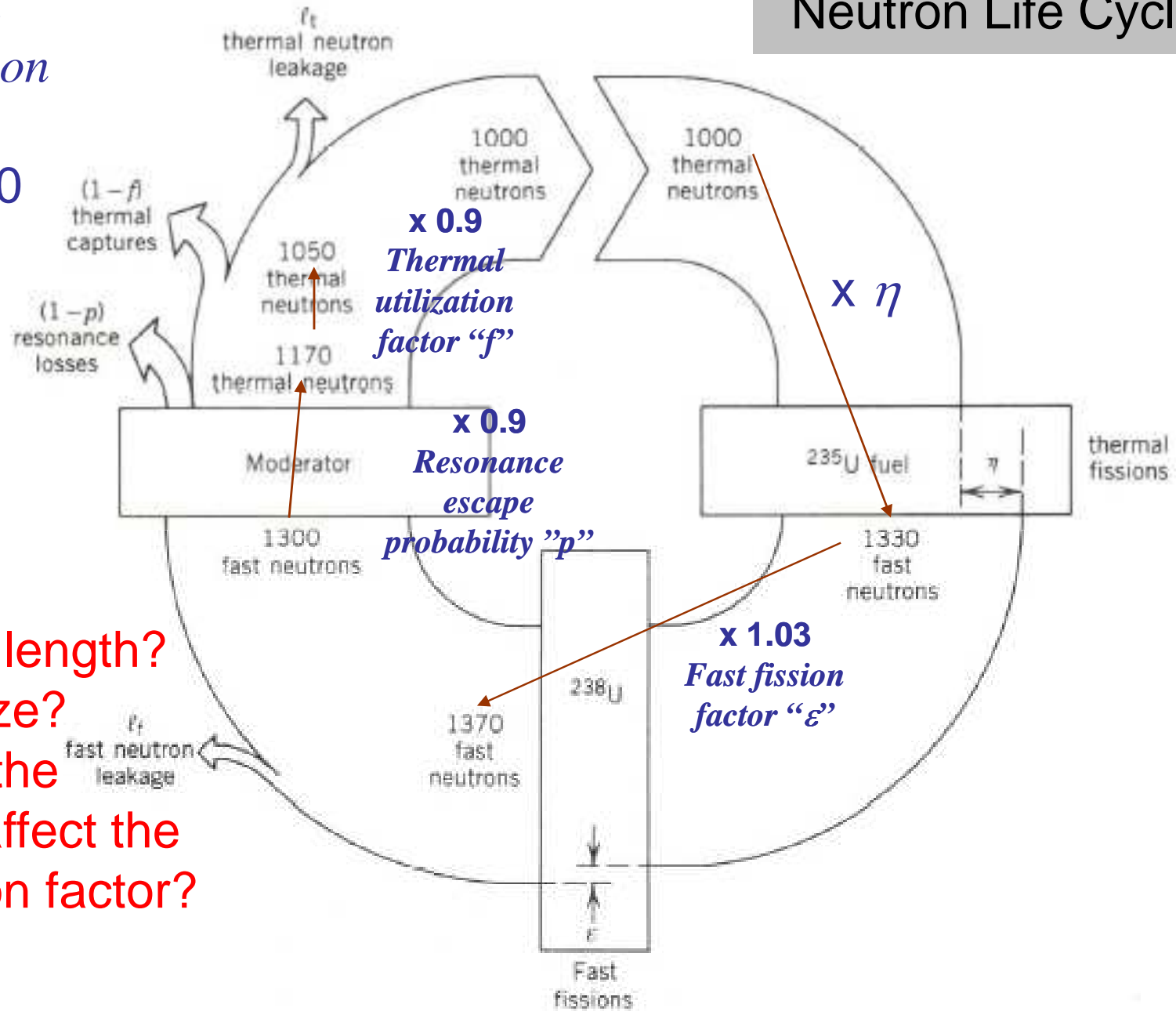
- Thermal available for fuel $f = \frac{\Sigma_a^{fuel}}{\Sigma_a^{fuel} + \Sigma_a^{clad} + \Sigma_a^{moderator} + \Sigma_a^{rods} + \Sigma_a^{poison} + \dots}$

Thinking QUIZ

- For each thermal neutron absorbed, how many fast neutrons are produced? Will need this when discuss two-group diffusion.

Neutron Life Cycle

Neutron
reproduction
factor
 $k = 1.000$



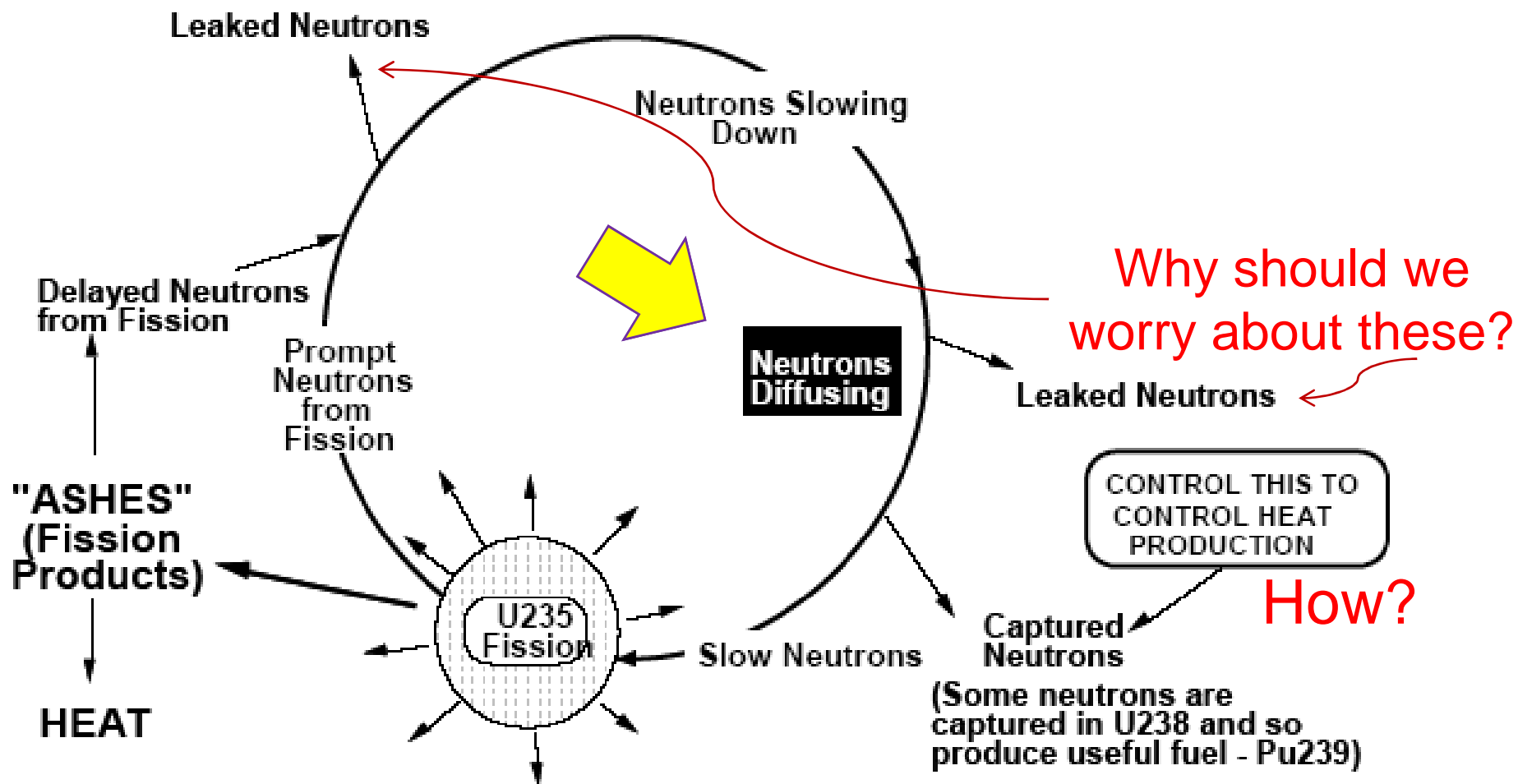
What is:

- Migration length?

- Critical size?

How does the geometry affect the reproduction factor?

Neutron Life Cycle



Controlled Fission

$$k = fp\varepsilon\eta(1-l_{fast})(1-l_{thermal}) \quad \text{Not fixed...!}$$

- Thermal utilization factor f can be changed, as an example, by adding absorber to coolant (PWR) (chemical shim, boric acid), or by inserting movable control rods in & out.
- Reactors can also be controlled by altering neutron leakages using movable neutron reflectors.
- f and p factors change as fuel is burned.
- f , p , η change as fertile material is converted to fissile material.

Controlled Fission

- Attention should be paid also to the fact that reactor power changes occur due to changes in resonance escape probability p . If Fuel $T \uparrow$, $p \downarrow$ *due to* Doppler broadening of resonance peaks.

Under-moderation
and
over-moderation.

